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OPTIMAL DESIGN OF AN OPEN-ENDED BRAIDED STENT USING MOPSO

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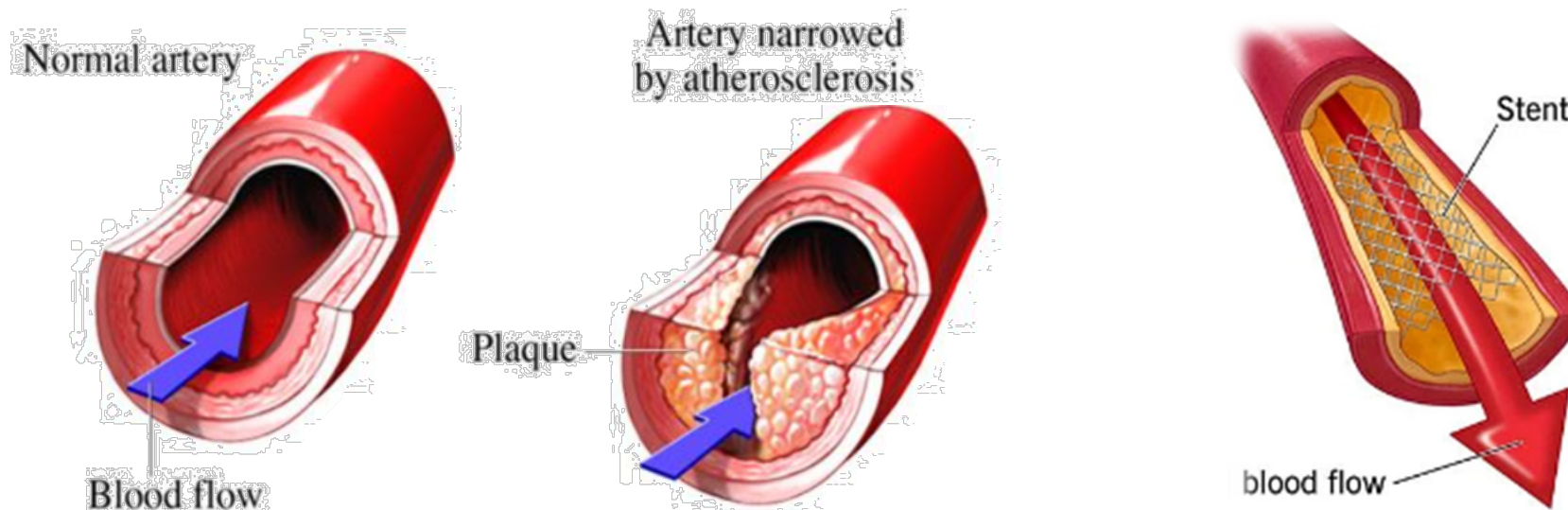
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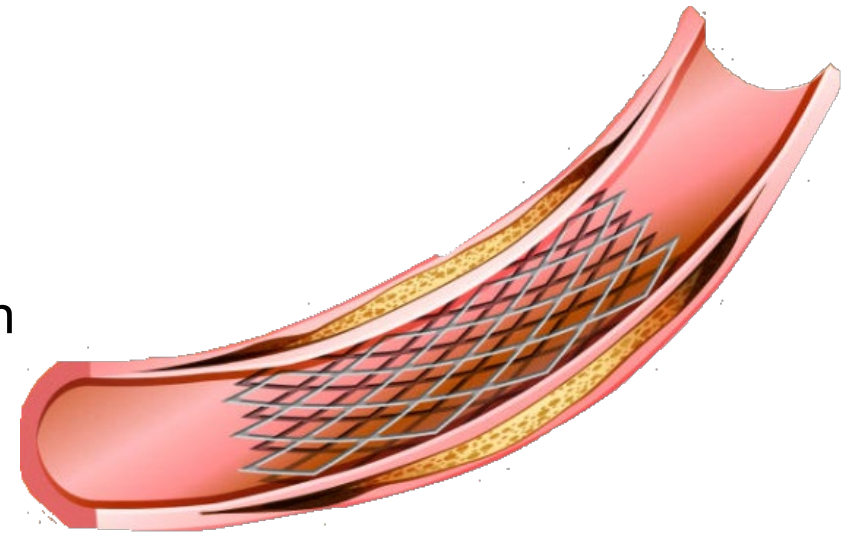
CORONARY ARTERY DISEASE

- **Atherosclerosis** : fat or lipid substances are deposited on the arterial wall
- Severe atherosclerosis cause coronary artery disease
- effective treatment method is Percutaneous Coronary Intervention (PCI)
- PCI is to unblock and restore blood by placing **vascular stent** on the stenosis



WHAT IS THE STENT ?

- A small meshlike device made of metal
- Acts as a support or scaffold in keeping the vessel open
- helps to improve blood flow to the heart muscle



Ideal Functions And Mechanical Properties of Stents

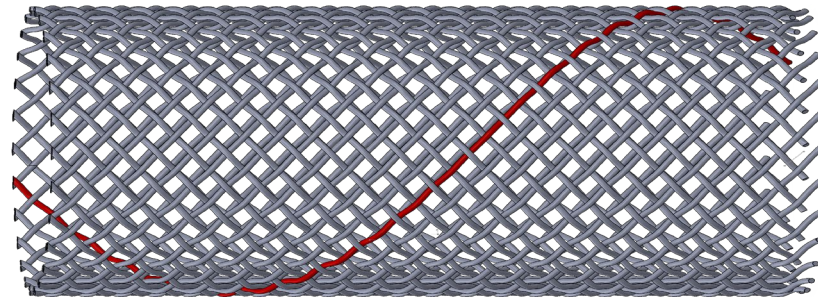
High Radial Stiffness **Maintain the vessel open and withstand the periodic load of arteries**

Minimum Foreshortening **Accurately placed in the position**

Maximum Radial Strength **Pushed away the blockage and better anchorage**

PROBLEM STATEMENT AND ASSUMPTIONS

1. Investigate a stent based on Edwards and Clerc study from technical literature
2. Using the MOPSO algorithm to **enhance mechanical properties**
3. Using AM to **reduce mass/cost** while maintaining mechanical performance

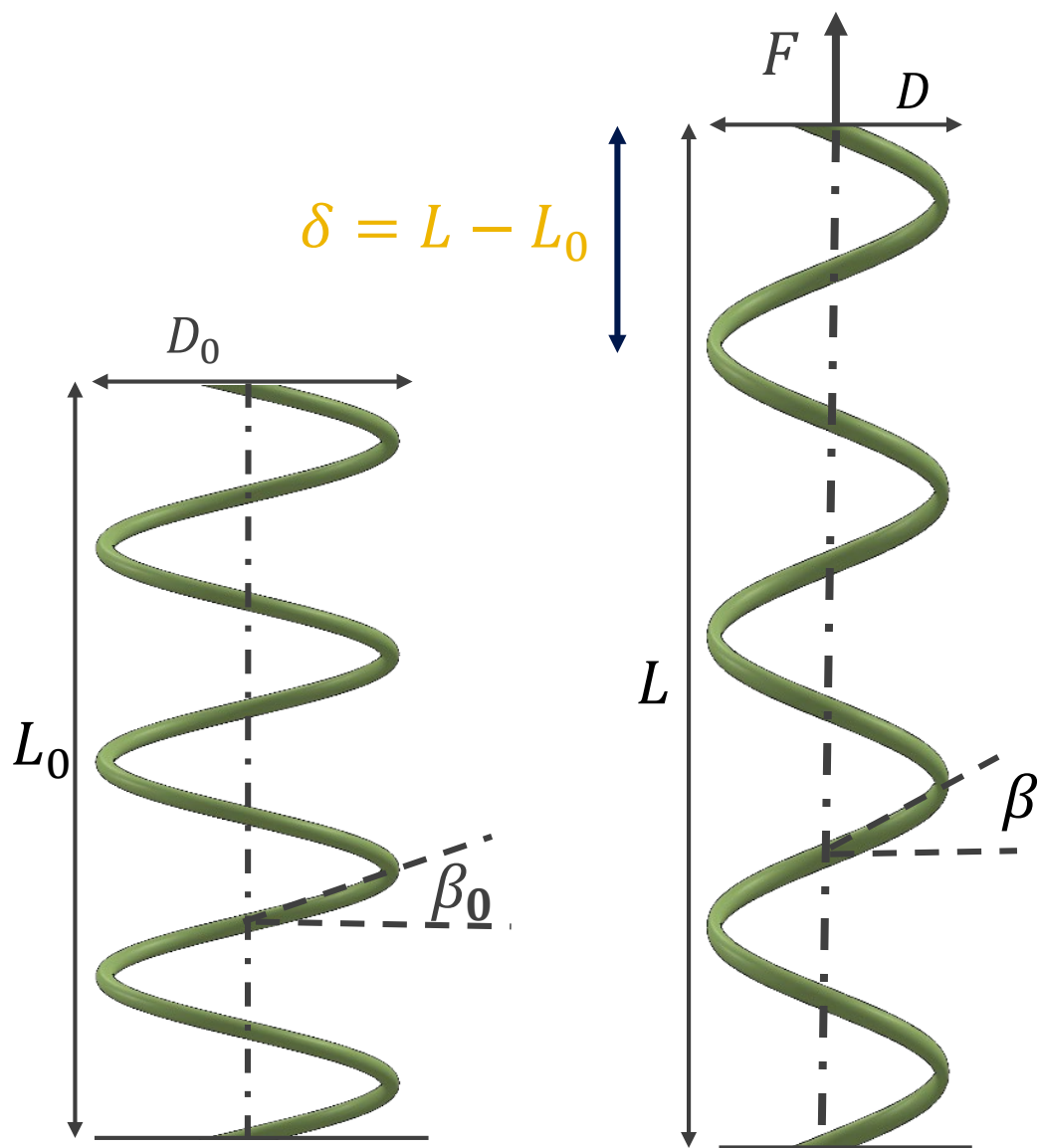


ASSUMPTION ON THE STENT BEHAVIOUR

- a) It acts as a collection of **independent open -coiled helical springs** .
- b) The ends are **fixed against rotating** around the longitudinal axis.
- c) It undergoes only **elastic deformation**



STENT GEOMETRY



INITIAL PITCH

$$p_0 = \pi D_0 \tan \beta_0$$

NUMBER OF COILS

$$c = L_0 / p_0$$

STENT DIAMETER

$$D = \frac{D_0 \cos(\beta)}{\cos(\beta_0)}$$

STENT LENGTH

$$L = \frac{L_0 \sin(\beta)}{\sin(\beta_0)}$$

MATERIAL

Linear elastic steel



MECHANICAL PROPERTIES AND ANALYTICAL MODEL

The axial force F exerted on the stent

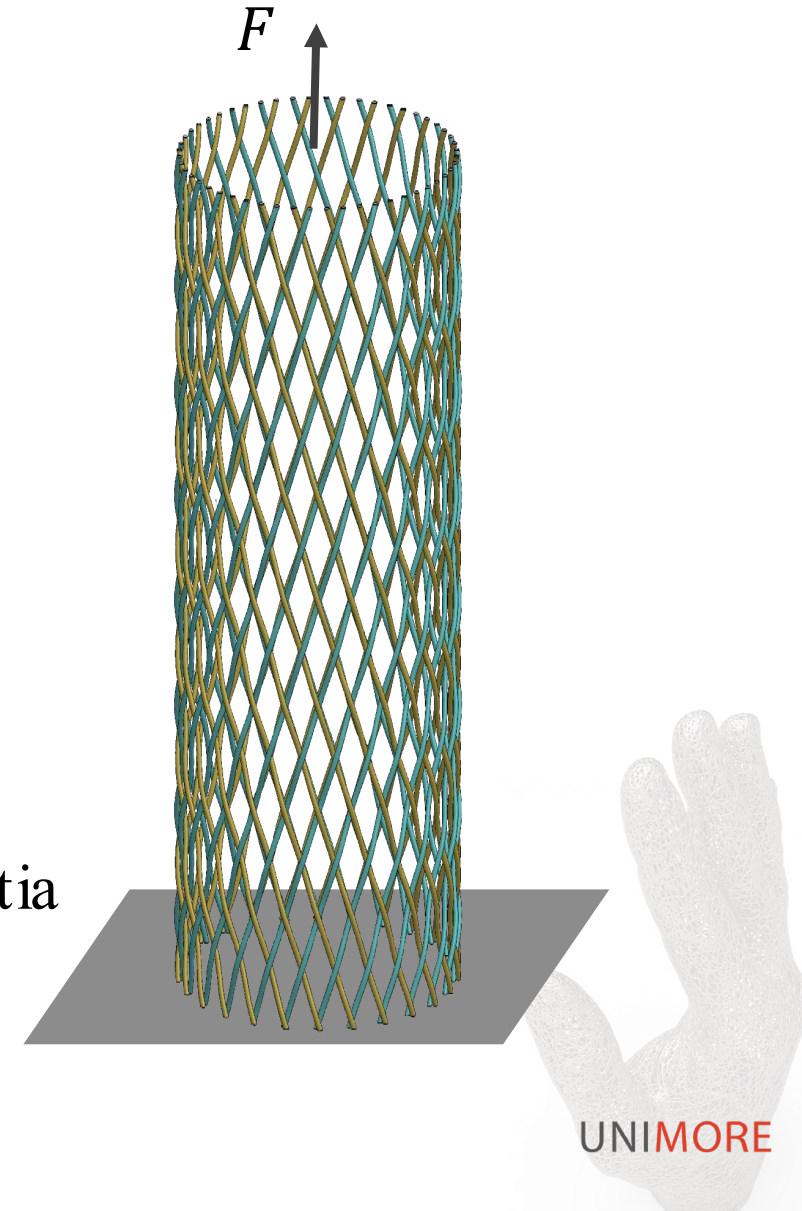
$$F = 2N \left[\frac{GI_P}{K_3} \left(\frac{2\sin(\beta)}{K_3} - K_1 \right) - \frac{EI \cdot \tan(\beta)}{K_3} \left(\frac{2\cos(\beta)}{K_3} - K_2 \right) \right]$$

$$K_1 = \frac{\sin(2\beta_0)}{D_0} \quad K_2 = \frac{2\cos^2(\beta_0)}{D_0} \quad K_3 = \frac{D_0}{\cos(\beta_0)}$$

N : the number of wires

I and I_P : the moment of inertia and polar moment of inertia

G and E : the shear modulus and Young's modulus

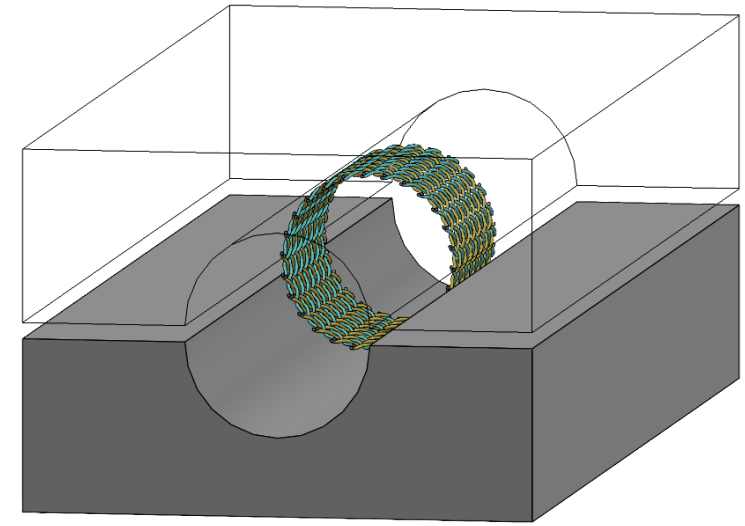


MECHANICAL PROPERTIES

$$dW = F \cdot d\delta \quad \rightarrow \quad F \cdot d\delta = P\pi DL \frac{dD}{2}$$

$$dW = P\pi DL \frac{dD}{2}$$

P and F perform the equal amount of work



RADIAL PRESSURE

$$P = \frac{2cF}{DL \tan(\beta)}$$

RADIAL FORCE

$$F_R = \frac{2\pi cF}{\tan(\beta)}$$

RADIAL PRESSURE STIFFNESS

$$K_P = \frac{dP}{dD} = \frac{dP}{d\beta} \cdot \frac{d\beta}{dD}$$

$$K_P = \frac{2c}{K_3 \sin(\beta) (DL \tan(\beta))^2} \times \left[\begin{array}{l} 2DLN \cdot \tan(\beta) \left(\frac{GI_p}{K_3} \left(\frac{2 \cos(\beta)}{K_3} \right) - \frac{EI}{K_3} \left(\frac{2 \cos(\beta)}{K_3} - \frac{K_2}{\cos^2(\beta)} \right) \right) \\ - F \left(\frac{DL}{\cos^2(\beta)} + K_3 \sin(\beta) \times (\pi cD - L \cdot \tan(\beta)) \right) \end{array} \right]$$

MECHANICAL PROPERTIES

Shear and bending stress (σ, τ)

$$\tau = \frac{F \cdot \cos(\beta) \cdot D/2 \cdot d/2}{I_p}$$

Twisting moment

$$\sigma = \frac{F \sin(\beta) \cdot D/2 \cdot d/2}{I}$$

Bending moment

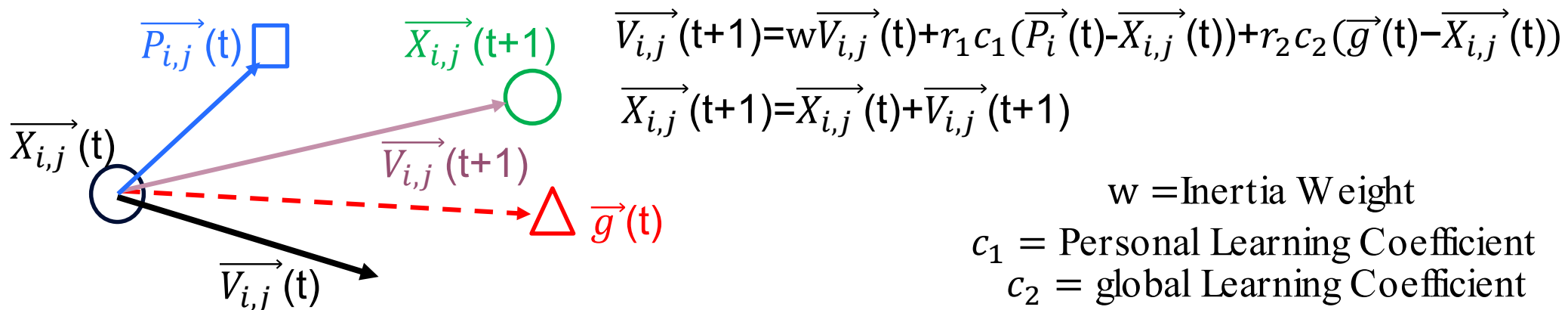


$$\sigma_{eq} = \sqrt{\frac{2\sigma^2 + 6\tau^2}{2}}$$



MULTI OBJECTIVE PARTICLE SWARM OPTIMIZATION

PSO Based on the paradigm of swarm intelligence, introduced by James Kennedy and Russell Eberhart in 1995



MOPSO Developed by Carlos et.al 2004

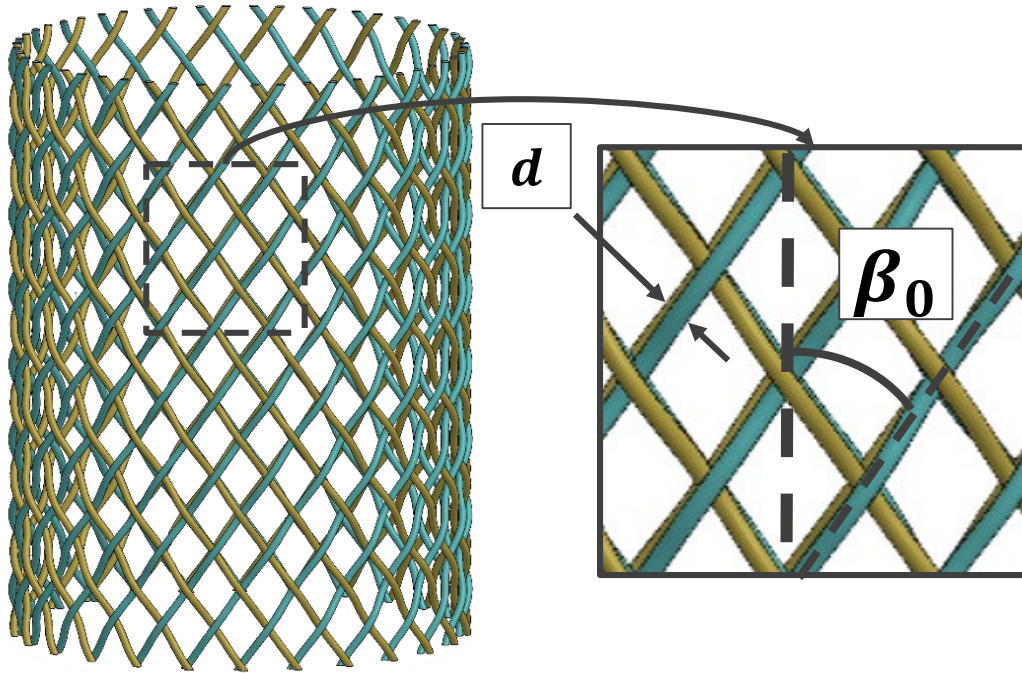
- Like PSO particles are sharing info. & moving towards global best particles and their own personal best memories.
- Unlike PSO there is more than one criterion to determine and define the best global.

Non-dominated particles



Repository

MULTI OBJECTIVE PARTICLE SWARM OPTIMIZATION



DESIGN VARIABLES

N = Number of wires
 β_0 = Initial pitch angle
 d = Diameter of the wire

COST FUNCTIONS

Minimize the maximum stent length

Maximize the radial Force exerted on the veins

Maximize the radial stiffness

$$V = N \cdot \frac{L_0}{\sin \beta_0} \cdot \pi d^2$$

CONSTRAINTS

$$V_{Optimized} \leq V_{Jedwab}$$

$$\sigma_{eq} < \text{yield strength}$$

$$\beta_{min} > \arctan \left(\frac{dN}{\pi D} \right)$$

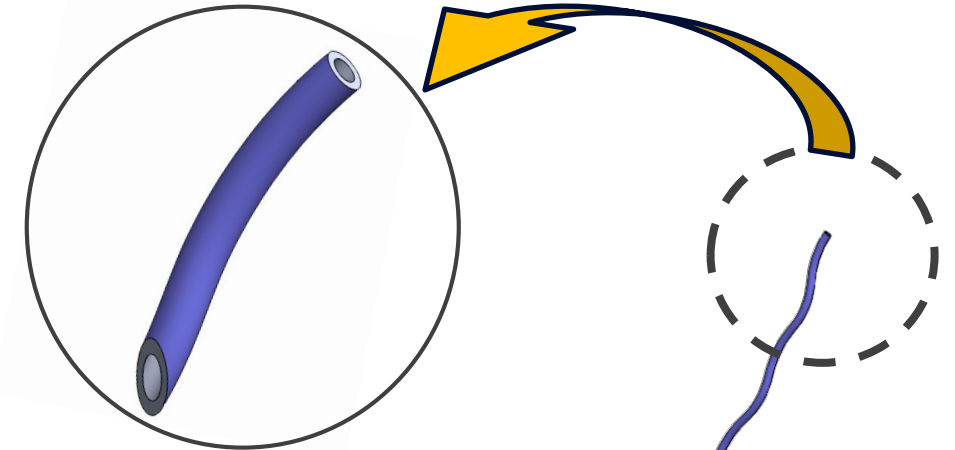
USE OF AM TO GET HOLLOW / LIGHTER STRUCTURE

t = Thickness

$$d_{in} = 2\left(\frac{d}{2} - t\right)$$

$$I_P = \frac{\pi}{32} (d^4 - d_{in}^4)$$

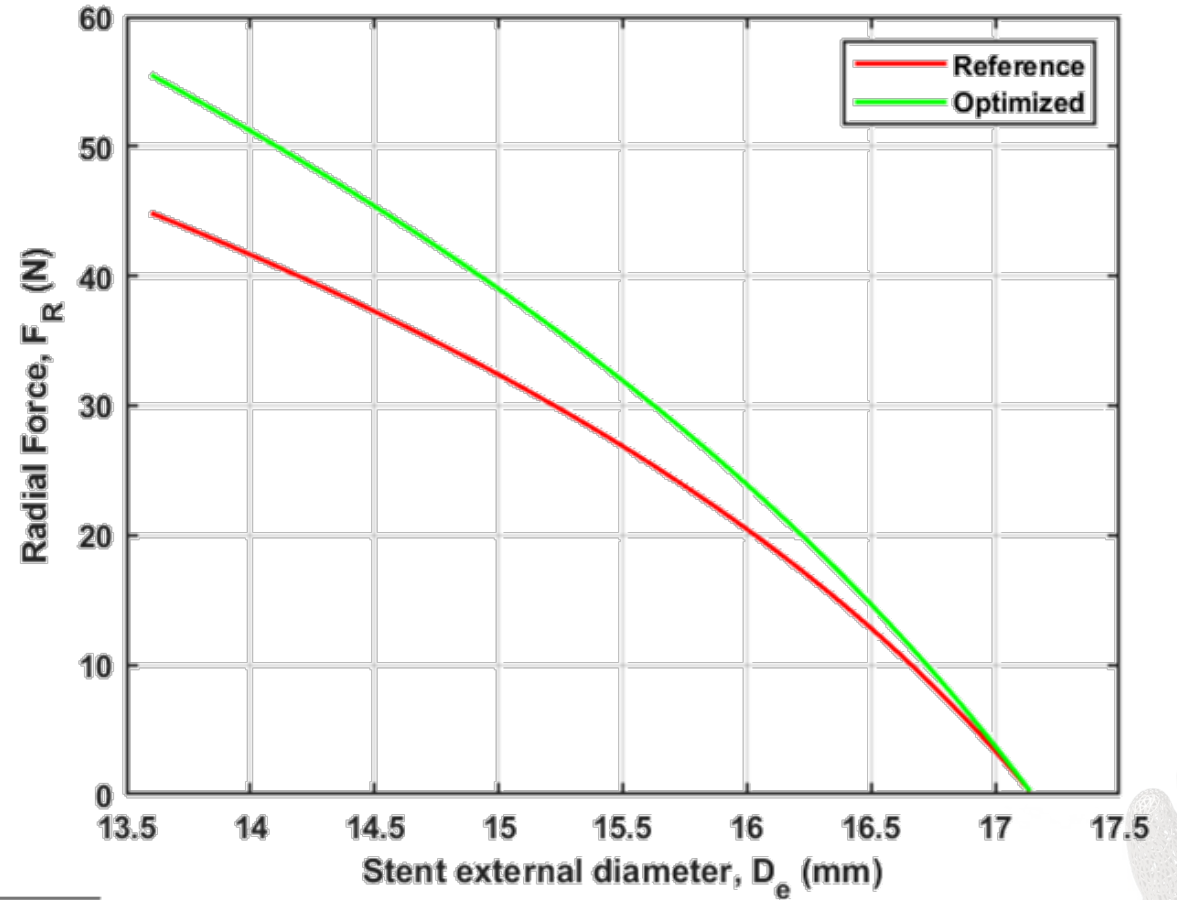
$$I = \frac{\pi}{32} (d^4 - d_{in}^4)$$



Method	Common material	Resolution
SLM	Stainless steels, aluminium (Al), copper (Cu), iron (Fe), cobalt (Co)-chrome (CR), Ti, Ni-based alloy, and a mixture of different types of particles (Fe, Ni, Cu, and Fe ₃ P)	20 μm
DED	Steel alloys, stainless steel, tool steel, Al, bronze, Co-Cr, (Fe, Ni)-TiC composites and Ti,	20 μm

RESULTS: RADIAL FORCE

Parameter	value
Initial average stent diameter D_0 (mm)	16.71
Wire diameter d (mm)	0.22
Number of wires N	24
Volume of the stent (mm^3)	673
Initial pitch angle β_0 ($^\circ$)	28.3
Initial stent length L_0 (mm)	87.5
Young's modulus E (MNm^{-2})	206000
Yield stress S_y (MNm^{-2})	2500



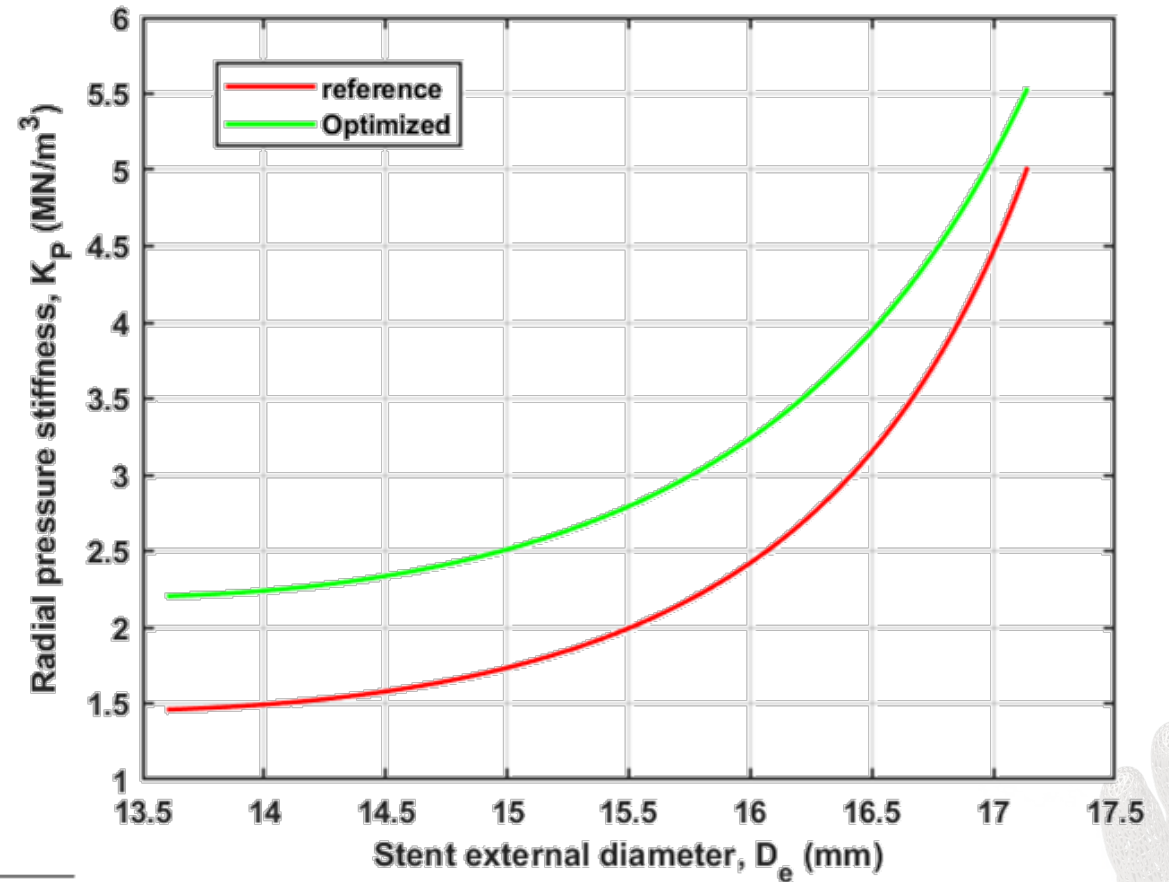
Design	N	d	β_0	$Volume$
Opt.1	18	0.266	31.54	670

D_0 (fully deployed) $\rightarrow 0.8D_0$

RESULTS: RADIAL PRESSURE STIFFNESS

Parameter	value
Initial average stent diameter D_0 (mm)	16.71
Wire diameter d (mm)	0.22
Number of wires N	24
Volume of the stent (mm^3)	673
Initial pitch angle β_0 ($^\circ$)	28.3
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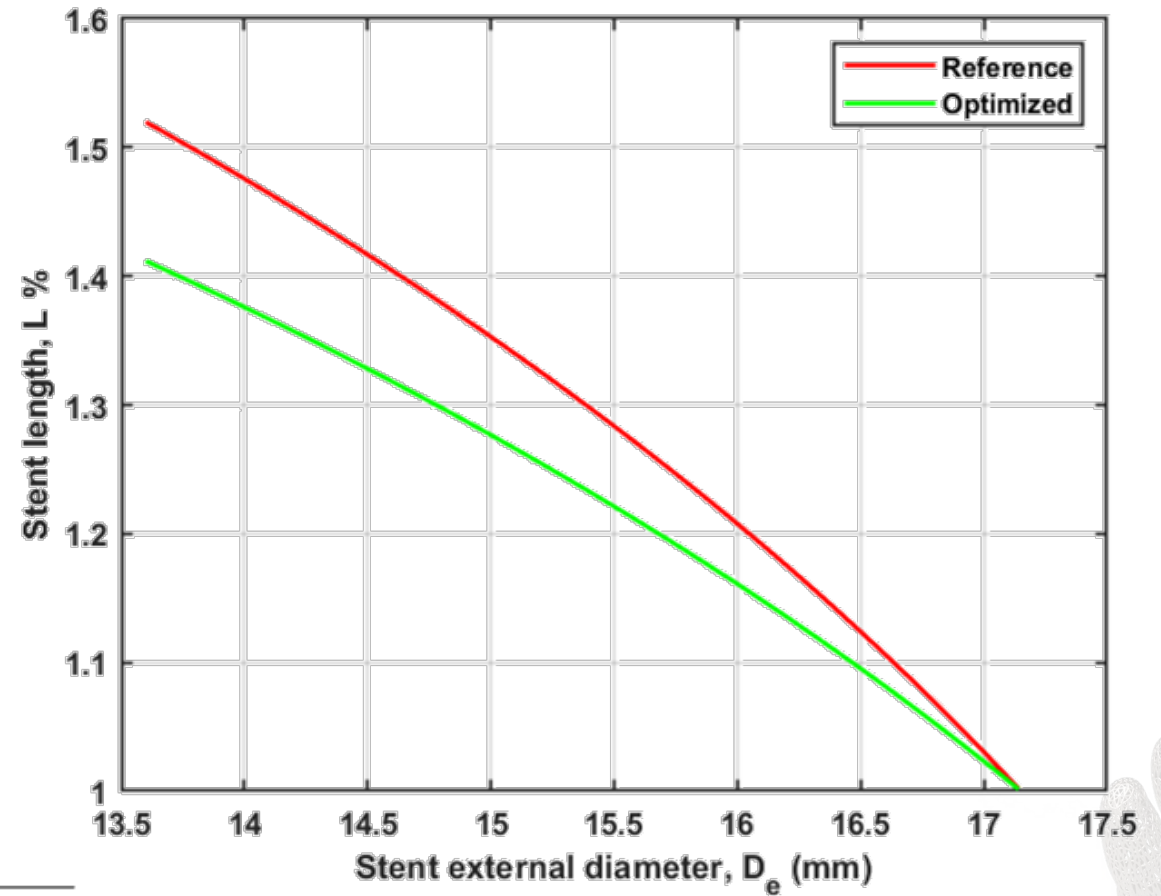


D_0 (fully deployed) $\rightarrow 0.8D_0$

RESULTS: STENT LENGTH

Parameter	value
Initial average stent diameter D_0 (mm)	16.71
Wire diameter d (mm)	0.22
Number of wires N	24
Volume of the stent (mm^3)	673
Initial pitch angle β_0 ($^\circ$)	28.3
Initial stent length L_0 (mm)	87.5
Young's modulus E (MNm^{-2})	206000
Yield stress S_y (MNm^{-2})	2500

Design	N	d	β_0	$Volume$
Opt.1	18	0.266	31.54	670



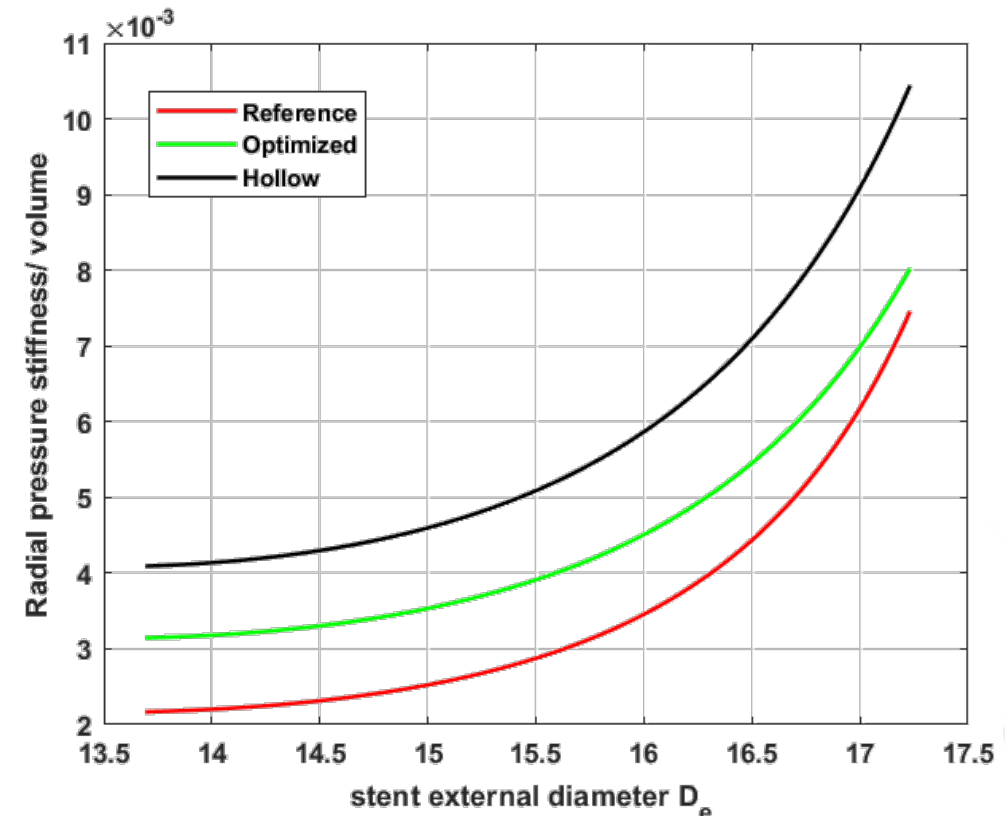
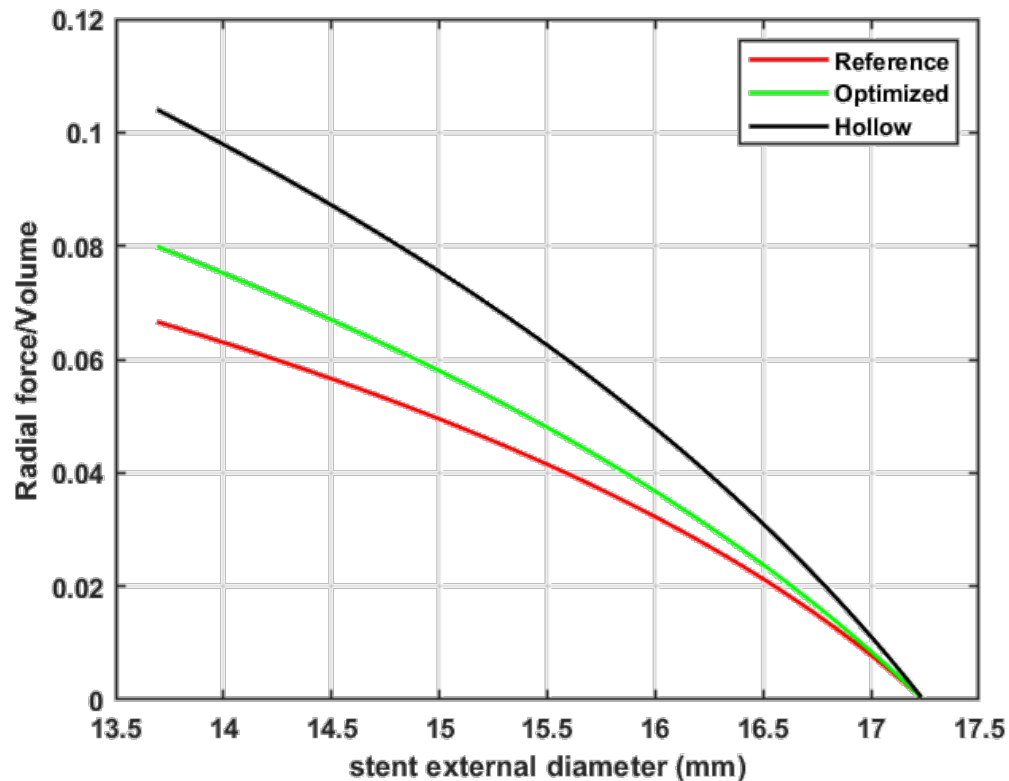
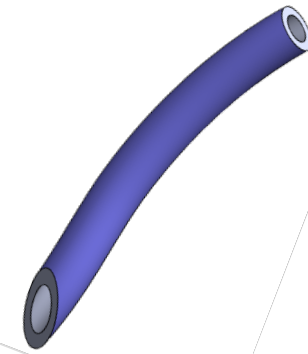
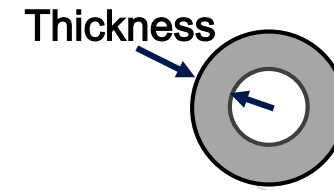
D_0 (fully deployed) $\rightarrow 0.8D_0$

AM TECHNOLOGY : 3D PRINTED HOLLOW WIRES

$$\text{Volume Reduction Ratio (VRR)} = \frac{\text{initial volume} - \text{final volume}}{\text{initial volume}} \times 100$$

Thickness = 60 μm

Final volume = 468 mm^3 \rightarrow **VRR = 30.17**



CONCLUSION & FUTURE DEVELOPMENT

1. Optimize the performance of an open ended braided stent
2. Analytical approach + MOPSO optimization
3. Specific radial force F_r , specific radial pressure stiffness K_p , are optimized
4. F_r and K_p increased especially for lower diameters
5. The stent's maximum length is reduced from 1.51% to 1.41%.
6. A 3D-printed hollow structure is envisioned
7. According to the optimization stent's weight is lowered 30%.
8. Future steps: extend the optimization to superelastic NiTi